



UPC - BARCELONA TECH  
MSc COMPUTATIONAL MECHANICS  
Spring 2018

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# Computational Solid Mechanics & Dynamics

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**ASSIGNMENT 5**

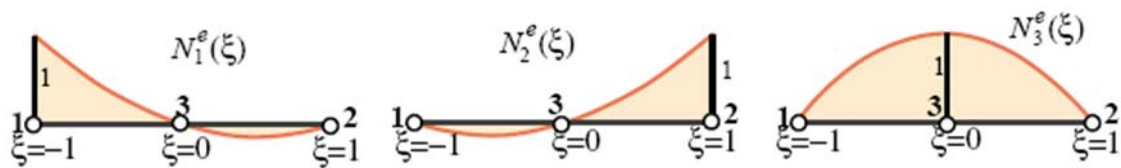
Due 12/03/2018

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**Problem 5.1**

Consider a three-node bar element referred to the natural coordinate  $\xi$ . The two end nodes and the mid node are identified as 1, 2 and 3 respectively. The natural coordinates of nodes 1, 2 and 3 are  $\xi = -1$ ,  $\xi = 1$  and  $\xi = 0$ , respectively. The variation of the shape functions  $N_1(\xi)$ ,  $N_2(\xi)$  and  $N_3(\xi)$  is sketched in the figure below. These functions must be quadratic polynomials in  $\xi$ :

$$N_1^e(\xi) = a_0 + a_1\xi + a_2\xi^2 \quad N_2^e(\xi) = b_0 + b_1\xi + b_2\xi^2 \quad N_3^e(\xi) = c_0 + c_1\xi + c_2\xi^2$$

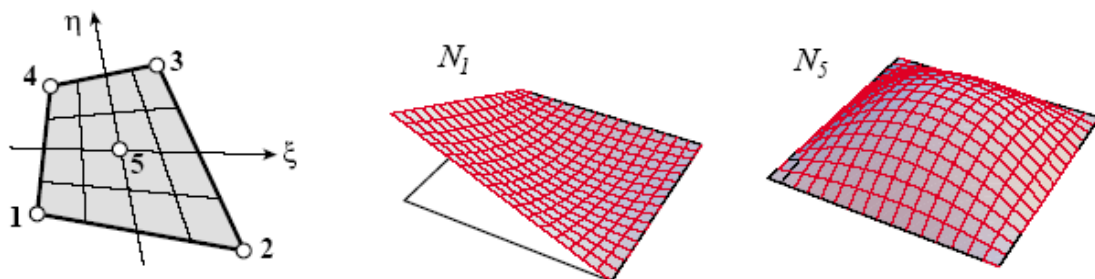


**Figure.-** Isoparametric shape functions for 3-node bar element (sketch).  
 Node 3 has been drawn at the 1-2 midpoint but it may be moved away from it.

- a) Determine the coefficients  $a_0, \dots, c_2$  using the node value conditions depicted in figure. For example  $N_1^e = 1$  for  $\xi=1$  and 0 for the rest of natural coordinates. The rest of the nodes follow the same scheme.
- b) Verify that their sum is identically one.
- c) Calculate their derivatives respect to the natural coordinates.

**Problem 5.2**

A five node quadrilateral element has the nodal configuration shown in the figure with two perspective views of  $N_1^e$  and  $N_5^e$ . Find five shape functions  $N_i^e$ ,  $i=1, \dots, 5$  that satisfy compatibility and also verify that their sum is unity.



Hint: develop  $N_5(\xi, \eta)$  first for the 5-node quad using the line-product method. Then the corner shape functions  $\underline{N}_i(\xi, \eta)$ ,  $i=1, 2, 3, 4$ , for the 4-node quad (already given in the notes). Finally combine  $N_i = \underline{N}_i + \alpha N_5$  determining  $\alpha$  so that all  $N_i$  vanish node 5. Check that  $N_1 + N_2 + N_3 + N_4 + N_5 = 1$  identically.

*Master of Science in Computational Mechanics 2018*  
**Computational Structural Mechanics and Dynamics**

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**“Convergence requirements”**

**Problem 5.3**

Which minimum integration rules of Gauss-product type gives a rank sufficient stiffness matrix for these elements:

1. the 8-node hexahedron
2. the 20-node hexahedron
3. the 27-node hexahedron
4. the 64-node hexahedron

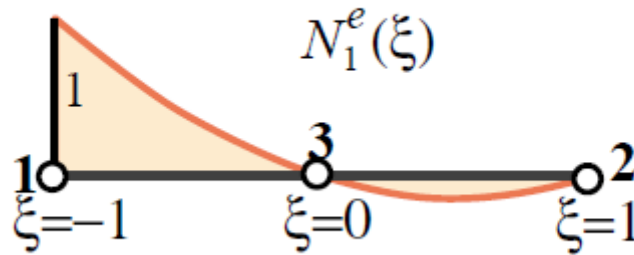
**Date of Assignment: 5 / 03 / 2018**

**Date of Submission: 12 / 03 / 2018**

The assignment must be submitted as a pdf file named **As5-Surname.pdf** to the CIMNE virtual center.

5.1 Consider a three node bar element to natural coordinate  $\zeta$ . The natural coordinate of nodes 1,2 and 3 are  $\zeta = -1, \zeta = 0$  and  $\zeta = 1$  respectively. These functions must be quadratic polynomials in  $\zeta$

a) For Node 1



$$N_1^e = a_0 + a_1\zeta + a_2\zeta^2$$

From the above figure it can be seen that the values for the shape function for node 1 are

$$N_1^e(\zeta = -1) = 1$$

$$N_1^e(\zeta = 0) = 0$$

$$N_1^e(\zeta = 1) = 0$$

If we use the values of node values at the natural coordinates we can find out values for constants  $a_0, a_1$  and  $a_2$

$$N_1^e(\zeta = -1) = 1 = a_0 - a_1 + a_2$$

$$N_1^e(\zeta = 0) = 0 = a_0$$

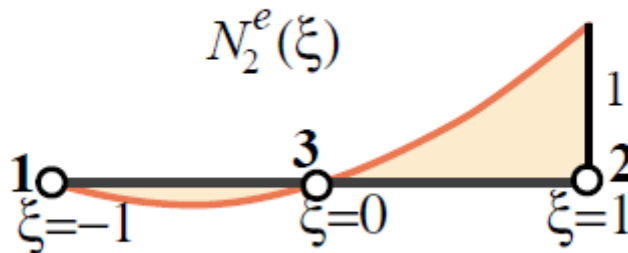
$$N_1^e(\zeta = 1) = 0 = a_0 + a_1 + a_2$$

Hence, the values for constants are as follows

$$a_0 = 0, a_1 = \frac{-1}{2}, a_2 = \frac{1}{2} \text{ Therefore the shape function for node 1 is}$$

$$N_1^e = \frac{-\zeta}{2} + \frac{\zeta^2}{2}$$

For Node 2



$$N_2^e = b_0 + b_1\zeta + b_2\zeta^2$$

From the above figure it can be seen that the values for the shape function for node 1 are

$$N_2^e(\zeta = -1) = 0$$

$$N_2^e(\zeta = 0) = 0$$

$$N_2^e(\zeta = 1) = 1$$

If we use the values of node values at the natural coordinates we can find out values for constants  $b_0, b_1$  and  $b_2$

$$N_2^e(\zeta = -1) = 0 = b_0 - b_1 + b_2$$

$$N_2^e(\zeta = 0) = 1 = b_0$$

$$N_2^e(\zeta = 1) = 0 = b_0 + b_1 + b_2$$

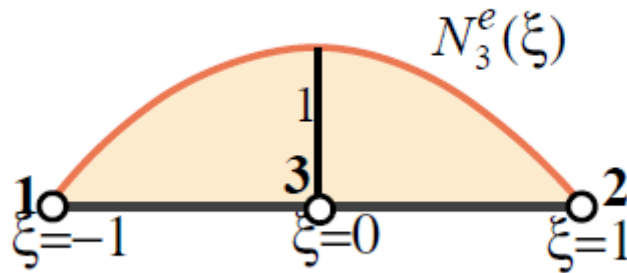
Hence, the values for constants are as follows

$$b_0 = 0, b_1 = b_2 = \frac{1}{2}$$

Therefore the shape function for node 2 is

$$N_2^e = \frac{\zeta}{2} + \frac{\zeta^2}{2}$$

For Node 3



$$N_3^e = c_0 + c_1\zeta + c_2\zeta^2$$

From the above figure it can be seen that the values for the shape function for node 1 are

$$N_3^e(\zeta = -1) = 0$$

$$N_3^e(\zeta = 0) = 1$$

$$N_3^e(\zeta = 1) = 0$$

If we use the values of node values at the natural coordinates we can find out values for constants  $c_0, c_1$  and  $c_2$

$$N_3^e(\zeta = -1) = 0 = c_0 - c_1 + c_2$$

$$N_3^e(\zeta = 0) = 1 = c_0$$

$$N_3^e(\zeta = 1) = 0 = c_0 + c_1 + c_2$$

Therefore the shape function for node 3 is

$$N_3^e = 1 - \zeta^2$$

b) Verify the sum of shape functions is one

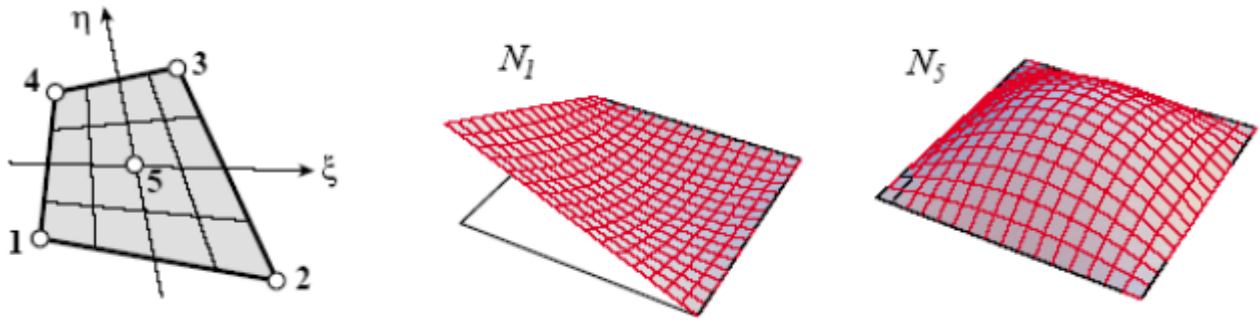
$$N_1^e + N_2^e + N_3^e = \left(\frac{-\zeta}{2} + \frac{\zeta^2}{2}\right) + \left(\frac{\zeta}{2} + \frac{\zeta^2}{2}\right) + (1 - \zeta^2) = 1$$

Hence it is verified that the sum of shape functions is 1. Thus proving that the shape functions satisfy compatibility equation

c) The derivatives with respect to natural coordinates

$$\begin{aligned}\frac{\partial N_1^e}{\partial \zeta} &= \frac{-1}{2} + \zeta \\ \frac{\partial N_2^e}{\partial \zeta} &= \frac{1}{2} + \zeta \\ \frac{\partial N_3^e}{\partial \zeta} &= -2\zeta\end{aligned}$$

**5.2 A five node quadrilateral element has the nodal configuration shown in the figure. To find shape functions for the same**



From the lecture notes, we already have the shape functions for the four corner nodes. Which are as follows

$$\begin{aligned}\underline{N}_1^e &= \frac{1}{4}(1 - \zeta)(1 - \eta) \\ \underline{N}_2^e &= \frac{1}{4}(1 + \zeta)(1 - \eta) \\ \underline{N}_3^e &= \frac{1}{4}(1 + \zeta)(1 + \eta) \\ \underline{N}_4^e &= \frac{1}{4}(1 - \zeta)(1 + \eta)\end{aligned}$$

We calculate the shape function for node 5 as follows

$$N_5(\zeta, \eta) = c_5(1 - \zeta)(1 - \eta)(1 + \zeta)(1 + \eta) = c_5(1 - \zeta^2)(1 - \eta^2)$$

From the figure it is clear that the value of  $N_5$  at various natural coordinates

$$N_5(0, 0) = c_5(1 - 0^2)(1 - 0^2)$$

$$\therefore c_5 = 1$$

$$\therefore \boxed{N_5 = (1 - \zeta^2)(1 - \eta^2)}$$

It can be seen from the figure that for 4 node quadrilateral that shape function for nodes 1, 2, 3, 4 does not become zero at node 5. Hence we combine  $N_i = \underline{N}_i + \alpha N_5$ , determining  $\alpha$  so that all  $N_i$  vanish at node 5. This simply means that we modify the shape functions of 4 node quadrilateral so that shape functions for respective nodes (1, 2, 3, 4) become zero at natural coordinates (0,0).  $N_i = \underline{N}_i + \alpha N_5$

$$N_1 = \underline{N}_1 + \alpha N_5 = \frac{1}{4}(1 - \zeta)(1 - \eta) + \alpha(1 - \zeta^2)(1 - \eta^2)$$

For node 1, the value of  $N_1$  is zero at node 5 (0,0).

$$0 = \frac{1}{4}(1 - 0)(1 - 0) + \alpha(1 - 0^2)(1 - 0^2)$$

$\therefore \alpha = -\frac{-1}{4}$  From the above equation and repeating this calculation for each node it is found out that the value of alpha for each node shape function is  $\frac{-1}{4}$ . Therefore the new shape functions for 5 node quadrilateral are as follows

$$\begin{aligned} N_1 &= \frac{1}{4}(1 - \zeta)(1 - \eta) - \frac{1}{4}(1 - \zeta^2)(1 - \eta^2) \\ N_2 &= \frac{1}{4}(1 + \zeta)(1 - \eta) - \frac{1}{4}(1 - \zeta^2)(1 - \eta^2) \\ N_3 &= \frac{1}{4}(1 + \zeta)(1 + \eta) - \frac{1}{4}(1 - \zeta^2)(1 - \eta^2) \\ N_4 &= \frac{1}{4}(1 - \zeta)(1 + \eta) - \frac{1}{4}(1 - \zeta^2)(1 - \eta^2) \\ N_5 &= (1 - \zeta^2)(1 - \eta^2) \end{aligned}$$

### 5.3 Finding minimum integration rules of Gauss Product type type gives a rank sufficient matrix for following elements

To solve this problem we are going to consider following terms

$n_F$  = number of element degrees of freedom

$n_R$  = number of independent rigid body modes

$r$  = rank of stiffness matrix  $K^e$

$n_E$  = order of stress strain matrix  $\mathbf{E}$ .

$n_G$  = minimum number of Gauss Points

We know that for an element to be rank sufficient,  $r = n_F - n_R$ . And furthermore if the we want to numerically integrate, and to attain rank sufficiency, the product  $n_E n_G \geq n_F - n_R$

Using all the above condition, the minimum Gauss point, and number of Gauss points actual used are calculated

1) 8 node hexahedron

$$n_F = 8 * 3 = 24$$

$$n_R = 6$$

$$n_E = 6$$

$$n_G = ?$$

$$r = n_F - n_R = 24 - 6 = 18$$

$$n_E n_G \geq n_F - n_R$$

$$6.n_G \geq 18$$

The minimum  $n_G = 3$

The minimum Gauss integration rule to be used for rank sufficiency is  $2 \times 2 \times 2$

2) 20 node hexahedron

$$n_F = 20 * 3 = 60$$

$$n_R = 6$$

$$n_E = 6$$

$$n_G = ?$$

$$r = n_F - n_R = 60 - 6 = 54$$

$$n_E n_G \geq n_F - n_R$$

$$6.n_G \geq 54$$

The minimum  $n_G = 9$

The minimum Gauss integration rule to be used for rank sufficiency is  $3 \times 3 \times 3$

3) 27 node hexahedron

$$n_F = 27 * 3 = 81$$

$$n_R = 6$$

$$n_E = 6$$

$$n_G = ?$$

$$r = n_F - n_R = 81 - 6 = 75$$

$$n_E n_G \geq n_F - n_R$$

$$6 \cdot n_G \geq 75 \text{ The minimum } n_G = 12.5$$

The minimum Gauss integration rule to be used for rank sufficiency is  $3 \times 3 \times 3$

4) 64 node hexahedron

$$n_F = 64 * 3 = 192$$

$$n_R = 6$$

$$n_E = 6$$

$$n_G = ?$$

$$r = n_F - n_R = 192 - 6 = 186$$

$$n_E n_G \geq n_F - n_R$$

$$6 \cdot n_G \geq 186 \text{ The minimum } n_G = 31$$

The minimum Gauss integration rule to be used for rank sufficiency is  $4 \times 4 \times 4$