

UNIVERSITAT POLITÈCNICA DE CATALUNYA
Master of Science in Computational Mechanics
Computational Structural Mechanics and Dynamics
CSMD
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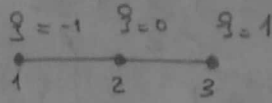
Assignment 5 - Isoparametric Representation and Convergence Requirements

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5.1

a) Given:



$$N_1(g) = a_0 + a_1 g + a_2 g^2, \quad N_2(g) = b_0 + b_1 g + b_2 g^2$$

$$N_3(g) = c_0 + c_1 g + c_2 g^2$$

for N_1 , the compatibility reads:

$$N_1(-1) = 1 = a_0 - a_1 + a_2$$

$$N_1(0) = 0 = a_0$$

$$N_1(1) = 0 = a_0 + a_1 + a_2$$

$$a_0 = 0; \quad 1 = 2a_2 \Rightarrow a_2 = \frac{1}{2} \Rightarrow a_1 = -\frac{1}{2}$$

thus:

$$N_1(g) = \frac{1}{2}(g-1)g$$

for N_2 , the compatibility reads:

$$N_2(-1) = 0 = b_0 - b_1 + b_2$$

$$N_2(0) = 1 = b_0$$

$$N_2(1) = 0 = b_0 + b_1 + b_2$$

$$b_0 = 1; \quad -2 = 2b_2 \Rightarrow b_2 = -1; \quad b_1 = 0$$

thus:

$$N_2(g) = 1 - g^2$$

for N_3 , the compatibility reads:

$$N_3(-1) = 0 = c_0 - c_1 + c_2; \quad c_0 = 0; \quad 2c_2 = 1 \Rightarrow c_2 = \frac{1}{2} \Rightarrow c_1 = \frac{1}{2}$$

$$N_3(0) = 0 = c_0$$

$$N_3(1) = 1 = c_0 + c_1 + c_2$$

thus:

$$N_3(g) = \frac{1}{2}(g+1)g$$

b)

$$\begin{aligned}
 N_1(s) + N_2(s) + N_3(s) &= \frac{1}{2}(s-1)s + (1-s^2) + \frac{1}{2}(s+1)s \\
 &= \frac{1}{2}s^2 - \frac{s}{2} + 1 - s^2 + \frac{s}{2} + \frac{1}{2}s^2 \\
 &= \frac{1}{2}s^2 + \frac{1}{2}s^2 - s^2 + 1
 \end{aligned}$$

$$N_1(s) + N_2(s) + N_3(s) = 1$$

c)

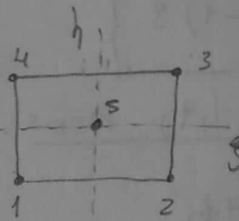
$$\frac{dN_1}{ds} = \frac{d}{ds} \left(\frac{1}{2}s^2 - \frac{1}{2}s \right) = s - \frac{1}{2}$$

$$\frac{dN_2}{ds} = \frac{d}{ds} (1 - s^2) = -2s$$

$$\frac{dN_3}{ds} = \frac{d}{ds} \left(\frac{s^2}{2} + \frac{s}{2} \right) = s + \frac{1}{2}$$

5.2

by the line method we propose:



$$N_s(s, h) = C_1 L_{1-2} \dots L_{4-1}$$

$$N_s(s, h) = C_1 L_{1-2} L_{2-3} L_{3-4} L_{4-1}$$

where:

$$\text{along } L_{1-2} : h = -1 \Rightarrow L_{1-2} = h + 1$$

$$\text{along } L_{2-3} : s = 1 \Rightarrow L_{2-3} = s - 1$$

$$\text{along } L_{3-4} : h = 1 \Rightarrow L_{3-4} = h - 1$$

$$\text{along } L_{4-1} : s = -1 \Rightarrow L_{4-1} = s + 1$$

thus:

$$N_s = C_1 (1+s)(1-s)(1+h)(1-h)$$

for compatibility

$$N_5(0,0) = 1 = C_1 \Rightarrow C_1 = 1$$

$$N_5 = (1+s)(1-s)(1+h)(1-h)$$

$$\boxed{N_5 = (1-s^2)(1-h^2)}$$

for the 4 corner modes we have:

$$\bar{N}_1 = C_1 L_{2-3} L_{4-3} = C_1 (s-1)(h-1)$$

$$\bar{N}_1(-1,-1) = 1 = 4C_1 \Rightarrow C_1 = \frac{1}{4}$$

$$\boxed{\bar{N}_1 = \frac{1}{4}(1-s)(1-h)}$$

$$\bar{N}_2 = C_2 L_{3-4} L_{4-1} = C_2 (s+1)(h-1)$$

$$\bar{N}_2(1,-1) = 1 = -4C_2 \Rightarrow C_2 = -\frac{1}{4}$$

$$\boxed{\bar{N}_2 = \frac{1}{4}(1+s)(1-h)}$$

$$\bar{N}_3 = C_3 L_{4-1} L_{1-2} = C_3 (1+s)(1+h)$$

$$\bar{N}_3(1,1) = 1 = 4C_3 \Rightarrow C_3 = \frac{1}{4}$$

$$\boxed{\bar{N}_3 = \frac{1}{4}(1+s)(1+h)}$$

$$\bar{N}_4 = C_4 L_{1-2} L_{2-3} = C_4 (s-1)(1+h)$$

$$\bar{N}_4(-1,1) = 1 = -4C_4 \Rightarrow C_4 = -\frac{1}{4}$$

$$\boxed{\bar{N}_4 = \frac{1}{4}(1-s)(1+h)}$$

for full compatibility N_1, N_2, N_3 and N_4 must vanish at mode 5:
using the hierarchical correction technique we can write:

$$N_i = \bar{N}_i + \alpha N_5 = \frac{1}{4}(1-s)(1-h) + \alpha(1-s^2)(1-h^2)$$

$$N_1(0,0) = 0 = \frac{1}{4} + \alpha \Rightarrow \alpha = -\frac{1}{4}$$

Same α value is found for N_2, N_3 and N_4 :

thus:

$$N_1 = \frac{1}{4}(1-s)(1-h) - \frac{1}{4}(1-s^2)(1+h^2)$$
$$= \frac{1}{4}(1-s)(1-h) - \frac{1}{4}(1-s)(1-h)(1+s)(1+h)$$

$$N_1 = \frac{1}{4}(1-s)(1-h) [1 - (1+s)(1+h)]$$

$$N_2 = \frac{1}{4}(1+s)(1-h) - \frac{1}{4}(1+s)(1-h)(1-s)(1+h)$$

$$N_2 = \frac{1}{4}(1+s)(1-h) [1 - (1-s)(1+h)]$$

$$N_3 = \frac{1}{4}(1+s)(1+h) - \frac{1}{4}(1+s)(1+h)(1-s)(1-h)$$

$$N_3 = \frac{1}{4}(1+s)(1+h) [1 - (1-s)(1-h)]$$

$$N_4 = \frac{1}{4}(1-s)(1+h) - \frac{1}{4}(1-s)(1+h)(1+s)(1-h)$$

$$N_4 = \frac{1}{4}(1-s)(1+h) [1 - (1+s)(1-h)]$$

$$N_5 = (1-s^2)(1-h^2)$$

- Interpolation condition is now satisfied by all $N_i(s, h)$
- Local support condition is also fulfilled by N_1, N_2, N_3 and N_4 as they vanish in boundaries where i node doesn't appear
- Inter-element compatibility condition is proved also, as follows:

$$\text{for } N_1 \text{ at } L_{1-2} \quad \eta = \text{cte} = -1 \Rightarrow N_1 = \frac{1}{2}(1-s) \quad (\text{Linear})$$

$$N_1 \text{ at } L_{4-1} \quad s = \text{cte} = -1 \Rightarrow N_1 = \frac{1}{2}(1-h) \quad (\text{Linear})$$

for N_2 : at L_{1-2} $\eta = -1 \Rightarrow N_2 = \frac{1}{2}(1+s)$ (Linear)

at L_{2-3} $s = 1 \Rightarrow N_2 = \frac{1}{2}(1-h)$ (Linear)

for N_3 : at L_{2-3} $s = 1 \Rightarrow N_3 = \frac{1}{2}(1+h)$ (Linear)

at L_{4-3} $h = 1 \Rightarrow N_3 = \frac{1}{2}(1+s)$ (Linear)

for N_4 : at L_{4-3} $h = 1 \Rightarrow N_4 = \frac{1}{2}(1-s)$ (Linear)

at L_{4-1} $s = -1 \Rightarrow N_4 = \frac{1}{2}(1+h)$ (Linear)

• thus, at boundaries all $N_i(s, h)$ are linear functions (1st order) which requires 2 nodes:

• the summation of the shape functions is given by:

$$N_1 + N_2 + N_3 + N_4 + N_5 = \frac{1}{4}(1-s)(1-h) - \frac{1}{4}(1-s^2)(1-h^2) + \frac{1}{4}(1+s)(1-h) - \frac{1}{4}(1-s^2)(1-h^2) + \frac{1}{4}(1+s)(1+h) - \frac{1}{4}(1-s^2)(1-h^2) + \frac{1}{4}(1-s)(1+h) - \frac{1}{4}(1-s^2)(1-h^2) + (1-s^2)(1-h^2) N_5$$

$$N_1 + N_2 + N_3 + N_4 + N_5 = \frac{1}{4}[(1-s)(1-h) + (1+s)(1-h) + (1+s)(1+h) + (1-s)(1+h)] + (1-s^2)(1-h^2) \left[1 - \frac{1}{4} - \frac{1}{4} - \frac{1}{4} - \frac{1}{4} \right]$$

$$= \frac{1}{4} \left\{ (1-s) [(1-h) + (1+h)] + (1+s) [(1-h) + (1+h)] \right\}$$

$$= \frac{1}{4} [2(1-s) + 2(1+s)] = \frac{1}{4} (2+2) = 1$$

thus:

$$\sum_{i=1}^5 N_i = 1$$

5.3

Given that, for a rank sufficiency elemental stiffness matrix we have:

$$r = m_f - m_R$$

where m_f is the number of degrees of freedom of the element, and m_R the number of independent rigid body modes.

As each Gauss point adds m_E to the rank of \underline{K}^e , to attain Rank Sufficiency, a numerical integration by Gauss quadrature must use a number of Gauss points m_G such that

$$m_E m_G \geq m_f - m_R$$

here we define m_E as the rank of the elasticity matrix denoted as \underline{E} .

1) 8-node hexahedron

• 3D element

• $m_E = 6$ (\underline{E} is a 6×6 matrix)

• $m_f = 3 \times 8 = 24$ (3 degree of freedom per node)

• $m_R = 6$ (3 rotations and 3 translations)

thus:

$$r = m_f - m_R = 24 - 6 = 18$$

$$6 m_G \geq 18 \Rightarrow m_G \geq 3$$

hence: a Gauss rule 1x1x1 provides Rank Sufficient matrix

2) 20-node hexahedron

$$m_E = 6$$

$$m_R = 6$$

$$m_f = 3 \times 20 = 60$$

thus:

$$r = m_f - m_R = 60 - 6 = 54$$

$$6 m_G \geq 54$$

$$m_G \geq 9$$

hence: a Gauss rule 2x2x2 gives only 8 points, then, a Gauss rule 3x3x3 is necessary

3) 27-Node hexahedron

$$m_E = 6$$

$$m_R = 6$$

$$m_f = 3 \times 27 = 81$$

thus:

$$r = m_f - m_R = 81 - 6 = 75$$

$$6MG \geq 75$$

$$MG \geq 12,5$$

hence, again a Gauss rule 3x3x3 is needed

4) 64-Node hexahedron

$$m_E = 6$$

$$m_R = 6$$

$$m_f = 3 \times 64 = 192$$

thus:

$$r = m_f - m_R = 192 - 6 = 186$$

$$6MG \geq 186$$

$$MG \geq 31$$

hence, a Gauss quadrature rule $3 \times 3 \times 3$ only provides

$MG = 27$, thus a Gauss rule 4x4x4 is needed